

# Effect of Al<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> on the structure and properties of porous forsterite-spinel-periclase ceramics

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### **01** Research Background



China has promised to reach the peak of  $CO_2$  emissions before 2030 and strive to achieve carbon neutrality before 2060. Energy conservation, emission reduction and improvement of thermal efficiency are ways to achieve "carbon neutrality".

# The world is hungry for ENERGY





Shaping

Sintering



Application



Fig. 1 Current status of refractory materials technology

# **01** Research Background



Fig. 2 Conventional structure of a high-temperature industrial furnace [1].

a) c) d)

Fig. 3 Examples of two different classes of porous ceramics used as high-temperature thermal insulators [2].

The heat storage loss of the furnace lining and the heat dissipation from the surface of the furnace body account for 1/4 to 1/2 of the total fuel consumption of industrial furnaces, resulting in significant heat loss in thermal furnaces.

# Research Method



# We use a novel method to fabricate **Porous Forsterite-Spinel-Periclase Ceramics(M-M2S-MA)**.





# **03** Experimental Results

Phase Evolution





Table 1 Chemical composition of raw materials (wt%).				
Composition of raw materials / wt%				
Sample no.	4MgCO <sub>3</sub> • Mg(OH) <sub>2</sub> •5 H <sub>2</sub> O	Al(OH) <sub>3</sub>	SiO <sub>2</sub>	- Or
S1	26	38	36	
a) J			b) Pore	

Fig. 6 SEM results of S1 pellet calcined at 1350 °C for 2 h.

100 um

20 um



Fig. 7 XRD patterns of samples after sintering at 1250-1600 °C: (a) S1A and (b) S1S (c) MAS1.

 $Al_2O_3(l) + MgO(s) \rightarrow MgAl_2O_4(s)$ (1)Liquid phase reaction:  $SiO_2(l) + MgO(s) \rightarrow Mg_2SiO_4(s)$ (2)



### **03** Experimental Results

Microstructure Evolution



Figure. 9 Microstructure images and EDS mappings of MAS1, S1A and S1S samples sintered at 1600 °C





Fig. 10 Physical properties of MAS1, S1A and S1S samples after sintered at 1600 °C : (a) BD and AP, (b) CCS, (c) Thermal <sup>2024-10-28</sup> conductivity values, (d) Pore size distribution of S1A, S1S and MAS1 samples sintered at 1600 °C

# **03** Experimental Results



Spinel: 7.6×10<sup>-6</sup>/K; Forsterite: 11.3×10<sup>-6</sup> K<sup>-1</sup> Periclase: 13.5×10<sup>-6</sup>/K

The thermal expansion coefficient of a composite material is related to the thermal expansion coefficients of its constituent components as well as the relative content of each crystal phase.

Fig. 11 Thermal expansion coefficient of samples sintered at 1600 °C.



Fig. 12 (a) Thermal shock resistance of samples MAS1, S1A and S1S, (b)Refractoriness under load of MAS1, S1A and S1S samples sintered at 1600 °C.

# **04** Conclusions and Significance

- 1. Adding 13.5 wt%  $\alpha$ -Al2O3 to the porous material increased magnesia-alumina spinel content after calcination, enhancing its room temperature compressive strength to 72.11 MPa, with a volume density of 1.90 g/cm3 and porosity of 42.8%.
- 2. Incorporating 8 wt% silica increased forsterite content to 75 wt%, forming a skeleton structure that improved high-temperature properties. The composite material has a volume density of 1.93 g/cm3, porosity of 42.6%, and a load softening temperature of 1618 °C.
- 3. The S1S sample with a higher forsterite content and larger grain size forms a skeletal structure, enhancing the material's load softening temperature, demonstrating the potential to improve refractory properties through phase and pore structure adjustments.





