

The 9th International Symposium on Refractories

# Comparative study on microstructures and properties of Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub>-C ceramic filter and Al<sub>2</sub>O<sub>3</sub>-C ceramic filter

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# — PART ONE — ① 武候科技大学

# **Research background**





Under the background of "Made in China 2025" policy, the demand for ultra-clean steel in major equipment manufacturing and major engineering construction in China is increasing day by day.

Non-metallic inclusion in steel is one of the important factors that affects steel properties and safety applications. Therefore, how to reduce the non-metallic inclusions and improve the quality of steel is a problem that needs to be solved at present.



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The porous ceramic filter has a threedimensional network structure, a porosity of up to 70-90%, and a large surface area, mainly used in the final procedure of steel casting, which is one of the effective ways to adsorb and filter the non-metallic inclusions in molten steel.



| <b>CaO filter</b> → Easy hydra                    | tion SiC filter                                    | -> Low filtration efficiency       |                 |
|---|--|------------------------------------|-----------------|
| $Zr_2O$ filter $\rightarrow$ Poor volum           | ne stability Al <sub>2</sub> O <sub>3</sub> filter | Poor thermal shock resistance      |                 |
| $Al_2O_3$ -C filter $\rightarrow \heartsuit$ Exce | llent filtration performance                       | ce, thermal shock resistance and c | reep resistance |
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### The inherent limitations of the Al<sub>2</sub>O<sub>3</sub>-C materials

In the aspect of sintering of strut, carbon is an inert phase in sintering theory, and it is difficult to form a strong neck bond between carbon and Al<sub>2</sub>O<sub>3</sub>, limiting the further enhancement of thermal shock resistance.



### Limit the further improvement of thermal shock resistance and strength!



In the other aspect of adsorption of inclusions, the smooth surface of dense Al<sub>2</sub>O<sub>3</sub> leads to a small contact area and contact angle with molten steel, thereby limiting the further improvement of inclusion adsorption and purification efficiency.

### Limit the further improvement of inclusion adsorption and purification efficiency!

厚惊惇學 崇室之谚 [1] Z. Chen, W. Yan, S. Schaffoner, Y.W. Li, M. Nath, C.Y. Zhu, Enhanced mechanical properties of lightweight Al2O3-C refractories reinforced by combined one-dimensional ceramic phases, Int. J. Appl. Ceram. Tec. 19 (3) (2022) 1613–1625.





### Firstly, pore is an important component of the microstructure.

| I MgO ceramic filter $$   | Physical properties   | PM               | FM                   |
|---|---|------------------|----------------------|
| Porous magnesia powder  | Bulk density of filter (g/cm <sup>3</sup> )                 | $0.91 \pm 0.01$  | $0.88 \pm 0.03$      |
| and the standard and the | Apparent porosity of filter (%)                             | 74.0 ± 0.01      | $74.1 \pm 0.03$      |
| MgO   | CCS (MPa)   | 1.71 ± 0.11      | <b>P</b> 1.46 ± 0.09 |
| MgO Pore  | CCS <sub>TS</sub> (MPa)                                     | $1.32 \pm 0.08$  | $1.08 \pm 0.05$      |
| 100 um  | Retention rate of CCS (%)                                   | 77.2             | 74.0                 |
| PM FM FM  | 1200 Steel reference with FM                                | cal compositions | of the steel samples |
|   | 14 800 -  | C (wt%)          | Al (wt%) T.O (ppm)   |
| Rougher surface   | Steel referen   | 0.100            | 0.250 37.5           |
|   | with F  | M 0.054          | 0.084 33.1           |
| Crack   | with P  | <b>M</b> 0.054   | 0.072 29.4           |
| 2000 µm CFACK   | 0-0.5 0.5-1 1-3 5-5 ≥5<br>Inclusion area (μm <sup>2</sup> ) |                  |                      |

厚惊懔 崇玄泛译 [2] Y. Liu, W. Yan, Z. Chen, J.F. Chen, Y. Liu, G.Q. Li, Preparation of high performance MgO ceramic filter and its interaction with molten steel: Effect of porous MgO powder, J. Eur. Ceram. Soc. 43 (8) (2023) 3794-3803.





Secondly, MgAl<sub>2</sub>O<sub>4</sub> is a crucial phase for enhancing the thermal shock resistance of MgO-Al<sub>2</sub>O<sub>3</sub> system materials.

### MgO-MgAl<sub>2</sub>O<sub>4</sub> ceramic filter



| Physical properties                        | MA0  | MA5  | MA10 | MA15 | MA20 |
|--|------|------|------|------|------|
| Bulk density of strut (g/cm <sup>3</sup> ) | 2.52 | 2.77 | 2.85 | 2.87 | 2.96 |
| Apparent porosity of strut (%)             | 28.8 | 22.3 | 20.4 | 20.1 | 17.0 |
| CCS (MPa)                                  | 1.68 | 2.04 | 1.78 | 1.84 | 2.35 |
| CCS <sub>TS</sub> (MPa)                    | 1.29 | 1.93 | 1.56 | 1.62 | 1.91 |
| Retention rate of CCS (%)                  | 76.7 | 94.6 | 87.6 | 88.0 | 81.3 |





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[3] Y. Liu, W. Yan, Y. Liu, Q. Wang, G.Q. Li, N. Li, Effect of α-Al2O3 content on microstructures, mechanical properties and purification efficiency on molten steel of MgO-based filters, J. Eur. Ceram. Soc. 43 (14) (2023) 6516–6526.
 [4] Z. Chen, W. Yan, G.Q. Li, S.S. Hong, N. Li, Enhanced mechanical properties of novel Al2O3-based ceramic filter by using microporous corundum-spinel and nano-Al2O3 powders, J. Eur. Ceram. Soc. 44 (2) (2024) 1070–1080.
 [5] Z. Chen, W. Yan, Y. Liu, G.Q. Li, S.S. Hong, N. Li, Purification performance on molten steel of novel Al2O3-based ceramic filter prepared from microporous powder and nano-Al2O3 powder, J. Iron Steel Res. Int. 31 (2024) 1535-1546.





Thirdly, the synergistic effect of the porous structure and  $\beta$ -SiC whiskers is an effective approach to enhancing the mechanical properties of Al<sub>2</sub>O<sub>3</sub>-C materials.

| Physical properties               | Aggregate T       | Aggregate M         |
|-----------------------------------|-------------------|---------------------|
| Bulk density (g/cm <sup>3</sup> ) | $3.54 \pm 0.02$   | $2.82 \pm 0.02$     |
| True density (g/cm <sup>3</sup> ) | $3.904 \pm 0.003$ | $3.967 {\pm} 0.003$ |
| Apparent porosity (%)             | 6.2±1             | 25.7±1              |
| Closed porosity (%)               | 3.1±1             | 3.2±1               |
| Total porosity (%)                | 9.3±1             | 28.9±1              |





| Physical properties of refractories  |      |      |  |  |  |
|--------------------------------------|------|------|--|--|--|
|                                      | TRS  | MRS  |  |  |  |
| Bulk density<br>(g/cm <sup>3</sup> ) | 2.87 | 2.66 |  |  |  |
| Apparent porosity<br>(%)             | 17.4 | 23.3 |  |  |  |
| CMOR (MPa)                           | 18.2 | 23.7 |  |  |  |



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[6] Z. Chen, W. Yan, S. Schaffoner, Y.J. Dai, Q. Wang, G.Q. Li, A novel approach to lightweight alumina-carbon refractories for flow control of molten steel, J. Am. Ceram. Soc. 103 (8) (2020) 4713–4724.
 [7] Z. Chen, W. Yan, S. Schaffoner, Y.W. Li, M. Nath, C.Y. Zhu, Enhanced mechanical properties of lightweight Al2O3-C refractories reinforced by combined one-dimensional ceramic phases, Int. J. Appl. Ceram. Tec. 19 (3) (2022) 1613–1625.







We propose the utilization of **porous**  $Al_2O_3$ -MgAl\_2O\_4 micropowder, high-reactive nano-carbon black, and Si powder to prepare the  $Al_2O_3$ -MgAl\_2O\_4-C filter. This approach aims to enhance thermal shock resistance through the synergistic toughening effects of  $\beta$ -SiC whiskers and the MgAl\_2O\_4 phase, while also improving the purification efficiency for molten steel by increasing the surface roughness of the filter's porous struts.

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# **Experiment procedures**



### **Experiment procedures**



|                        | Composition of the slurries   | s (wt%) |      |
|------------------------|---|---------|------|
|                        |   | AM      | А    |
|                        | Porous Al <sub>2</sub> O <sub>3</sub> -MgAl <sub>2</sub> O <sub>4</sub> micropowder | 80      | 0    |
|                        | α-Al <sub>2</sub> O <sub>3</sub> micropowder AMA-10                                 | 0       | 80   |
| Solids                 | Si  | 6       | 6    |
|                        | Carbores®P  | 6       | 6    |
|                        | Nano-Carbon Black N220  | 8       | 8    |
|                        | Carboxymethyl cellulose C804619   | 0.36    | 0.36 |
|                        | Lignosulfonate C804808  | 1.5     | 1.5  |
| Additives <sup>a</sup> | Polycarboxylate WSM-M   | 0.3     | 0.3  |
|                        | Glydol N1055  | 0.3     | 0.3  |
|                        | Contraspum K1012  | 0.1     | 0.1  |

#### Porous Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> raw material

Bulk density: 2.53 g/cm<sup>3</sup>; Apparent Porosity: 33.6% Prepared by **in situ decomposition pore-forming technique**<sup>[8-10]</sup>. The filters prepared with **porous Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> micropowder** were named **AM**.



#### Chemical composition of the raw materials (wt%)

|                                | $\alpha$ -Al <sub>2</sub> O <sub>3</sub> | Porous Al <sub>2</sub> O <sub>3</sub> -MgAl <sub>2</sub> O <sub>4</sub> |
|--------------------------------|--|---|
|                                | micropowder                              | micropowder   |
| $Al_2O_3$                      | 99.31                                    | 90.01   |
| MgO                            | 0.01                                     | 8.60  |
| SiO <sub>2</sub>               | 0.25                                     | 0.33  |
| CaO                            | 0.08                                     | 0.15  |
| Fe <sub>2</sub> O <sub>3</sub> | 0.07                                     | 0.41  |
| K <sub>2</sub> O               | 0.01                                     | 0.02  |
| Na <sub>2</sub> O              | 0.05                                     | 0.15  |
| TiO <sub>2</sub>               | 0.01                                     | 0.04  |
| IL                             | -  | 0.12  |

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[8] Z. Chen, W. Yan, S. Schafföner, J.N. Zhi, N. Li, Vacuum impregnation treatment of microporous Al2O3-MgAl2O4 refractory raw materials with sub-micron pores and high strength, J. Eur. Ceram. Soc. 42 (12) (2022) 5145–5152.
[9] W. Yan, G.Y. Wu, S.B. Ma, S. Schafföner, Y.J. Dai, Z. Chen, Energy efficient lightweight periclase-magnesium alumina spinel castables containing porous aggregates for the working lining of steel ladles, J. Eur. Ceram. Soc. 48 (12) (2018) 4276–4282.
[10] W. Yan, J.F. Chen, N. Li, W.D. Qiu, Y.W. Wei, B.Q. Han, Preparation and characterization of porous MgO-Al2O3 refractory aggregates using an in-situ decomposition pore-forming technique, Ceram. Int. 41 (1) (2015) 515–520



### **Experiment procedures**



### **Immersion experiment**

Al-killed steel (Wuhan Iron & Steel Co., China) was used in the immersion tests with a melting point of approximately 1540 °C and a composition of C 0.063 wt%, Al 0.46 wt%, Si 0.017 wt%, S 0.017 wt%, Mn 0.051 wt%. 200g of steel was used for each immersion experiment.

**The immersion experiment was performed in a highfrequency induction furnace in a rotating magnetic field.** The high purity **argon** with a purity of 99.99 % was slowly introduced with a flow rate of 0.5 L/min. When the temperature reached **1600** °C, the filter was slowly immersed in the molten steel for **20 min** before the filter was separated from the molten steel and furnace-cooled.



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### **Phase compositions (XRD results)**



Relative contents of phase in the specimens (wt%)

|   |    | Corundum | Spinel | β-SiC |
|---|----|----------|--------|-------|
| 1 | AM | 58       | 33     | 9     |
|   | Α  | 97       | -Q-V   | 3     |
| Ŀ |    |          |        |       |

### Morphologies of the filters



#### Surface roughness parameters of the substrates AM and A

|    | $R_q/\mu m$ | $R_a/\mu m$ | $R_z/\mu m$ | R <sub>SA</sub> |
|----|-------------|-------------|-------------|-----------------|
| AM | 0.799       | 0.626       | 3.055       | 1.072           |
| A  | 0.393       | 0.303       | 1.520       | 1.021           |
|    |             |             |             |                 |

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### **Microstructures of the filters**



### Physical properties of the filters

|   | AM               | Α                |
|---|------------------|------------------|
| Deally downsides of Citerry (m/arrow3)      |                  |                  |
| Buik density of filter (g/cm <sup>3</sup> ) | $0.76 \pm 0.05$  | 0.89±0.08        |
| Porosity of filter (%)                      | $57.30 \pm 2.81$ | $43.31 \pm 5.09$ |
| CCS (MPa)                                   | $0.45 \pm 0.10$  | $0.62 \pm 0.03$  |
| CCS <sub>TS</sub> (MPa)                     | $0.41 \pm 0.12$  | $0.36 \pm 0.13$  |
| <b>Retention rate of CCS (%)</b>            | 91.11            | 58.06            |

Filter AM exhibited a lower bulk density and a higher porosity. The cold compressive strength of filter A was 37.78% higher than that of filter AM. However, after three thermal shock tests, filter AM demonstrated a higher cold compressive strength than that of filter A. Specifically, filter AM retained 91.11% of its original strength, while filter A only retained 58.06%.

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### Interaction between the filters and molten steel



After immersion in the molten steel, filter AM retained integrity. Conversely, filter A experienced a complete fracture, with one half of the fractured specimen falling into the molten steel.

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| Chemical compositions of the steel specimens |         |          |          |           |  |  |  |  |
|--|---------|----------|----------|-----------|--|--|--|--|
|  | C (wt%) | Al (wt%) | Si (wt%) | T.O (ppm) |  |  |  |  |
| Steel reference                              | 0.063   | 0.46     | 0.017    | 56.3      |  |  |  |  |
| with AM                                      | 0.071   | 0.24     | 0.078    | 11.7      |  |  |  |  |
| with A                                       | 0.47    | 0.29     | 0.16     | 52.2      |  |  |  |  |



Filter AM reduced the T.O content from **56.3 ppm to 11.7 ppm**.

Filter A did not significantly reduce the T.O content, which was possibly related to its fracture and subsequent fall into the molten steel.







#### EDS results (At%)

|   | 0     | Mg    | Al    | Si    | Cr   | Fe    | Possible phases (1600°C)               |
|---|-------|-------|-------|-------|------|-------|--|
| 1 | 29.81 | 12.73 | 55.85 |       |      | 1.61  | Corundum, Spinel                       |
| 2 | 34.39 | 10.78 | 53.76 |       |      | 1.07  | Corundum, Spinel                       |
| 3 | 18.82 | 8.83  | 32.26 | 13.80 | 0.98 | 25.31 | Olivine, Corundum,<br>Composite Spinel |
| 4 | 43.04 | 9.28  | 41.74 | 5.94  |      |       | Corundum, Spinel,<br>Olivine           |
| 5 | 4.65  | 7.45  | 17.79 | 17.89 | 1.89 | 50.33 | Fe-Si-Al Alloy,<br>Composite Spinel    |

 $Al_2O_3$ -Mg $Al_2O_4$  reaction layer was observed on the surface of the filter, **exhibiting a significant distribution of micropores across its irregular surface.** It is observed that  $Al_2O_3$ -Mg $Al_2O_4$  and  $Al_2O_3$ -MgO-SiO<sub>2</sub> inclusions in the molten steel were adsorbed on the surface of the porous  $Al_2O_3$ -Mg $Al_2O_4$  layer.

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|   | EDS results (At%) |       |       |             |                          |  |  |  |
|---|-------------------|-------|-------|-------------|--------------------------|--|--|--|
|   | 0                 | Mg    | Al    | Si Fe       | Possible phases (1600°C) |  |  |  |
| 6 | 50.22             | 9.74  | 40.04 |             | Corundum, Spinel         |  |  |  |
| 7 |                   |       | 4.60  | 95.40       | ) Fe-Al Alloy            |  |  |  |
| 8 | 42.59             | 18.68 | 38.15 | 0.58        | Composite Spinel         |  |  |  |
| 9 |                   |       | 2.55  | 18.92 78.53 | 3 Fe-Si-Al Alloy         |  |  |  |

(a) The original layer, located far from the molten steel, retained its original morphology;

(b) The decarburized layer, located near the molten steel, **experienced intense carbothermal reduction reactions**, resulting in a loose structure;

(c) The  $Al_2O_3$ -Mg $Al_2O_4$  reaction layer, in **direct contact with the molten steel**, had a uniform thickness of approximately **27.2** µm.

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### Discussion

**Firstly**, porous  $Al_2O_3$ -Mg $Al_2O_4$  micropowder **facilitated the formation of \beta-SiC whiskers** within the filter.



| $2C(s)+O_2(g)=2CO(g)$            | (1) |
|----------------------------------|-----|
| $2Si(s)+O_2(g)=2SiO(g)$          | (2) |
| $SiO(g)+3CO(g)=SiC(s)+2CO_2(g)$  | (3) |
| $3SiO(g)+CO(g)=SiC(s)+2SiO_2(l)$ | (4) |
|                                  |     |

The  $\beta$ -SiC whiskers branched out and epitaxially grew, originating from the Fe catalyst droplets, forming a uniformly distributed  $\beta$ -SiC whisker network.

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### Discussion

Secondly, the  $\beta$ -SiC and MgAl<sub>2</sub>O<sub>4</sub> phase significantly enhanced the thermal shock resistance of the filter.

|    |    |     |    |              |     | •: Corundum<br>•: Spind<br>+: fl-SaC |     |    |  |
|----|----|-----|----|--------------|-----|--------------------------------------|-----|----|--|
| A  | мİ | Li. | Ŀ  | L            | li. | ii.                                  | i   |    |  |
| A  |    | L   | L  |              | L   | J.                                   | de. | ~  |  |
| 10 | 20 | 30  | 40 | 50<br>29 (*) | 60  | 70                                   | 80  | 90 |  |

| Porous Al <sub>2</sub> O <sub>3</sub> -MgAl <sub>2</sub> O <sub>4</sub> micropowder<br>(90.01 wt% Al <sub>2</sub> O <sub>3</sub> , 8.60 wt% MgO) |          |        |       |  |  |  |
|--|----------|--------|-------|--|--|--|
| Relative contents of phase (XRD results)   |          |        |       |  |  |  |
| Filter   | Corundum | Spinel | β-SiC |  |  |  |
| AM   | 58 wt%   | 33 wt% | 9 wt% |  |  |  |
| А  | 97 wt%   | -      | 3 wt% |  |  |  |
|  |          |        |       |  |  |  |

Filter AM exhibited a retention rate of 91.11% in its cold compressive strength after three thermal shock tests. The  $\beta$ -SiC whiskers interlocking porous Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> and carbon particles in the filter AM prevented the crack propagation during the immersion test, so that no large cracks occurred in the filter AM.









# **Discussion** Thirdly, the combination of the microporous structure and MgAl<sub>2</sub>O<sub>4</sub> phase synergistically improved the purification efficiency of the filter for molten steel.

**High purity argon** O<sub>2</sub> is less than 1ppm

 $P(O_2) \le 1*10^{-1} Pa$ 

Based on the experimental conditions, the process of interfacial reactions between filter AM and the molten steel will be discussed from the carbothermal reaction stage, the reaction layer formation stage and the final stage.



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Discussion

#### (a) Carbothermal reaction stage

**Carbothermal reaction stage** 

Mg Al Al<sub>2</sub>O AlO CO

Mg(g) Al(g) Al<sub>2</sub>O(g) AlO(g) CO(g)

 $Al_2O_3(s)+2C(s)=Al_2O(g)+2CO(g)$  $Al_2O_3(s)+C(s)=2AlO(g)+CO(g)$  $2Al_2O_3(s)+9C(s)=Al_4C_3(s)+6CO(g)$  $MgAl_2O_4(s)+4C(s)=Mg(g)+2Al(g)+4CO(g)$  $MgAl_2O_4(s)+3C(s)=Mg(g)+Al_2O(g)+3CO(g)$  $MgAl_2O_4(s)+2C(s)=Mg(g)+2AlO(g)+2CO(g)$  $2MgAl_2O_4(s)+11C(s)=2Mg(g)+Al_4C_3(s)+8CO(g)$ 

 $Al_2O_3(s)+3C(s)=2Al(g)+3CO(g)$ 



Al (g):  $6.3 \times 10^2$  Pa Al<sub>2</sub>O (g):  $9.7 \times 10^2$  Pa AlO (g): 5.2 Pa Mg (g):  $1.8 \times 10^3$  Pa CO (g):  $1.8 \times 10^3$  Pa

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**Growing point** 









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The filter AM had a rougher surface structure, where the aforementioned reaction process led to the formation of the Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> layer and FeAl<sub>2</sub>O<sub>4</sub> nuclei. As the inclusions were continuously and gradually adsorbed, the Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> layer progressively thickened, accompanied by the formation of acicular composite spinel on the surface. The Fe on the surface dissolved the Al and Si vapors to form Fe-Si-Al alloy spheres, which encapsulated the inclusions on the filter surface and linked with the porous layer through acicular composite spinel.

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### **Conclusions**

- $\bullet$  The porous Al<sub>2</sub>O<sub>3</sub>-MgAl<sub>2</sub>O<sub>4</sub> micropowder contained more  $Fe_2O_3$ . With the progress of VLS mechanism,  $\beta$ -SiC embryos formed on the rough grains surface under the catalysis of Fe, leading to the development of a network structure of β-SiC whiskers.
- $\bullet$  The β-SiC and MgAl<sub>2</sub>O<sub>4</sub> phase significantly enhanced the thermal shock resistance of the filter. After three thermal shock tests, the cold compression strength of filter AM (0.41 MPa) was higher than that of filter A (0.36 MPa), with a strength retention rate as high as 91.11%.
- The combination of the microporous structure and  $MgAl_2O_4$  phase synergistically improved the purification efficiency of the filter for molten steel.



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# Thank you for your listening!

PLEASE GIVE ME AS MUCH CRITICISM AS POSSIBLE

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